

# Statistical Modelling of Marine Turbulence

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# Contents

- Some theory of statistical turbulence modelling
- Mixing vs. stratification
- General Ocean turbulence Model (GOTM)
- Turbulence observations in the ocean
- Example: SIPS in Liverpool Bay
- Example: Convection in Lago Maggiore
- General Estuarine Transport Model (GETM)
- Example: Influx events in Arkona Sea

# Basic approaches

## Two approaches to averaged turbulence modelling:

- **Statistical turbulence modelling:** Convert NSE to Friedmann-Keller series, cut-off where suitable and parameterise unknown terms.
- **Empirical turbulence modelling:** Close equations on lowest order and parameterise relevant processes.

# NSE $\rightarrow$ Reynolds equation

Momentum Equation:

$$\partial_t v_i + v_j \partial_j v_i - \nu \partial_{jj} v_i + 2\varepsilon_{ijl} \Omega_j v_l = -\frac{\partial_i p}{\rho_0} - \frac{g_i}{\rho_0} \rho.$$

Reynolds averaging:

$$v_i = \bar{v}_i + \tilde{v}_i, \quad \rho = \bar{\rho} + \tilde{\rho}, \dots$$

Reynolds Equation:

$$\partial_t \bar{v}_i + \bar{v}_j \partial_j \bar{v}_i - \partial_j (\nu \partial_j \bar{v}_i - \langle \tilde{v}_j \tilde{v}_i \rangle) + 2\varepsilon_{ijl} \Omega_j \bar{v}_l = -\frac{\partial_i \bar{p}}{\rho_0} - g_i \frac{\bar{\rho}}{\rho_0}.$$

# Reynolds Stress Equation

$$\begin{aligned}
 & \partial_t \langle \tilde{v}_i \tilde{v}_j \rangle + \partial_l \left( \bar{v}_l \langle \tilde{v}_i \tilde{v}_j \rangle + \langle \tilde{v}_l \tilde{v}_i \tilde{v}_j \rangle - \nu \partial_l \langle \tilde{v}_i \tilde{v}_j \rangle \right) \\
 &= \underbrace{-\partial_l \bar{v}_i \langle \tilde{v}_l \tilde{v}_j \rangle - \partial_l \bar{v}_j \langle \tilde{v}_l \tilde{v}_i \rangle}_{P_{ij}} \\
 &\quad - \underbrace{2\Omega_l (\varepsilon_{ilm} \langle \tilde{v}_j \tilde{v}_m \rangle + \varepsilon_{jlm} \langle \tilde{v}_i \tilde{v}_m \rangle)}_{\Omega_{ij}} \\
 &\quad - \underbrace{\frac{1}{\rho_0} \{g_i \langle \tilde{v}_j \tilde{\rho} \rangle + g_j \langle \tilde{v}_i \tilde{\rho} \rangle\}}_{B_{ij}} - \underbrace{\frac{1}{\rho_0} (\langle \tilde{v}_i \partial_j \tilde{p} + \tilde{v}_j \partial_i \tilde{p} \rangle)}_{\Pi_{ij}} \\
 &\quad - \underbrace{2\nu \langle (\partial_l \tilde{v}_j) (\partial_l \tilde{v}_i) \rangle}_{\varepsilon_{ij}}.
 \end{aligned}$$

# Algebraic SMCs

The following steps lead to different types of second-moment closures:

- Empirical closures of pressure-strain correlators.
- Neglect or simplification of advective and diffusive fluxes of second-moments.
- Neglect of rotational terms in the second-moment equations.
- Boundary layer assumption (neglect of horizontal gradients and non-hydrostatic effects).
- ... and many more details ...

# Algebraic SMCs

## Turbulent Fluxes:

$$\langle \tilde{u}\tilde{w} \rangle = -\nu_t \partial_z \bar{u}, \quad \langle \tilde{w}\tilde{T} \rangle = -\nu'_t \partial_z \bar{T}$$

## Eddy Viscosity / Eddy Diffusivity:

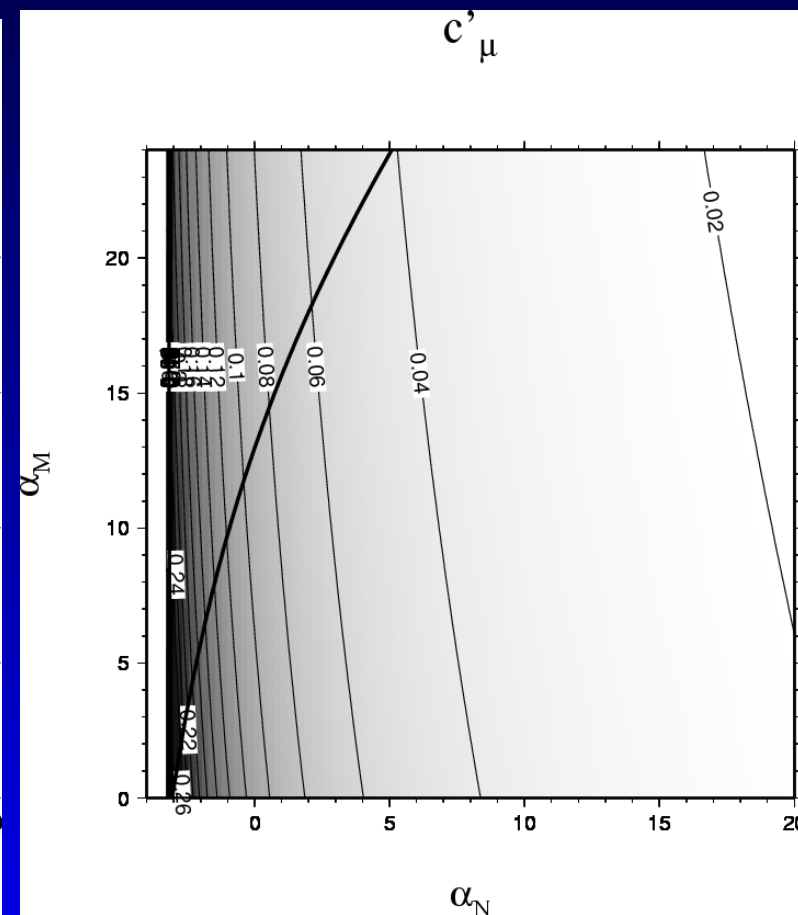
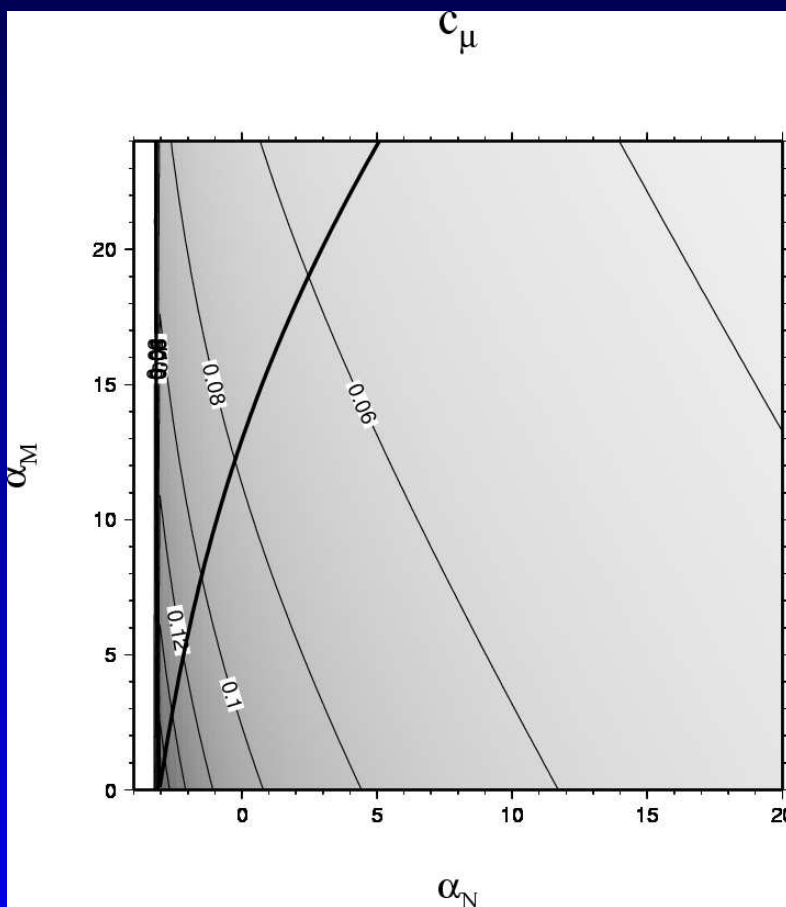
$$\nu_t = c_\mu(\alpha_M, \alpha_N) \frac{k^2}{\varepsilon}, \quad \nu'_t = c'_\mu(\alpha_M, \alpha_N) \frac{k^2}{\varepsilon}.$$

## Shear Number, Buoyancy Number:

$$\alpha_M = \frac{k^2}{\varepsilon^2} M^2, \quad \alpha_N = \frac{k^2}{\varepsilon^2} N^2.$$

# Stability Functions

Canuto et al. [2001]:



# Exact TKE-Equation

$$\begin{aligned} \partial_t k + \partial_j \left( \bar{v}_j k + \langle \tilde{v}_j \frac{1}{2} \tilde{v}_i^2 \rangle - \nu \partial_j k + \frac{1}{\rho_0} \langle \tilde{v}_j \tilde{p} \rangle \right) \\ = \underbrace{-\langle \tilde{v}_j \tilde{v}_i \rangle \partial_i \bar{v}_j}_P - \underbrace{\frac{g}{\rho_0} \langle \tilde{v}_3 \tilde{\rho} \rangle}_B - \underbrace{\nu \langle (\partial_j \tilde{v}_i)^2 \rangle}_\varepsilon, \end{aligned}$$

This TKE equation will be modelled as it is given above, the only parameterisations needed are for the **turbulent flux terms**, for which usually the down-gradient approximation is used.

# Dissipation equation

Exact form (e.g. *Wilcox [1998]*):

$$\begin{aligned}
 & \partial_t \varepsilon + \partial_j \left( \bar{v}_j \varepsilon + \langle \tilde{v}_j \nu (\partial_j \tilde{v}_i)^2 \rangle - \nu \partial_j \varepsilon + 2 \frac{\nu}{\rho_0} \langle \partial_i \tilde{v}_j \partial_i \tilde{p} \rangle \right) \\
 &= \underbrace{-2\nu \partial_j \bar{v}_i \left( \langle \partial_i \tilde{v}_k \partial_j \tilde{v}_k \rangle + \langle \partial_k \tilde{v}_i \partial_k \tilde{v}_j \rangle \right) - 2\nu \partial_{jk} \bar{v}_i \langle \tilde{v}_k \partial_j \tilde{v}_i \rangle}_{P_\varepsilon} \\
 & \quad \underbrace{-2\nu \frac{g}{\rho_0} \partial_j \langle \tilde{v}_3 \partial_j \tilde{\rho} \rangle}_{B_\varepsilon} - \underbrace{2\nu \left( \langle \partial_j \tilde{v}_i \partial_k \tilde{v}_i \partial_j \tilde{v}_k \rangle + \nu \langle (\partial_{ij} \tilde{v}_k)^2 \rangle \right)}_{\varepsilon_\varepsilon}
 \end{aligned} \tag{1}$$

$k$ - $\varepsilon$  model (*Launder and Spalding [1972]*):

$$\partial_t \varepsilon - \partial_z \left( \frac{\nu_t}{\sigma_\varepsilon} \partial_z \varepsilon \right) = \frac{\varepsilon}{k} (c_{\varepsilon 1} P + c_{\varepsilon 3} B - c_{\varepsilon 2} \varepsilon).$$

# Mellor-Yamada model

General relation between  $k$ ,  $\varepsilon$  and  $L$ :

$$L = c_{\mu}^{3/4} \frac{k^{3/2}}{\varepsilon}$$

$k$ - $kL$  model (Mellor and Yamada [1982]):

$$\partial_t (kL) - \partial_z (S_l \partial_z (kL)) =$$

$$\frac{L}{2} \left[ E_1 P + E_3 B - \left( 1 + E_2 \left( \frac{L}{L_z} \right)^2 \right) \varepsilon \right].$$

# Length scale equations (cont'd)

Other approaches are using equations for  $\omega = \varepsilon/k$  ( $k$ - $\omega$  model),  $k/\varepsilon$ ,  $k^2/\varepsilon$ , ..., so why not using the generalised approach of a  $k^n \varepsilon^m$  equation ?

Generic length scale equation  
(*Umlauf and Burchard [2003]*):

$$\partial_t (k^n \varepsilon^m) - \partial_z \left( \frac{\nu_t}{\sigma_{nm}} k^n \varepsilon^m \right) =$$

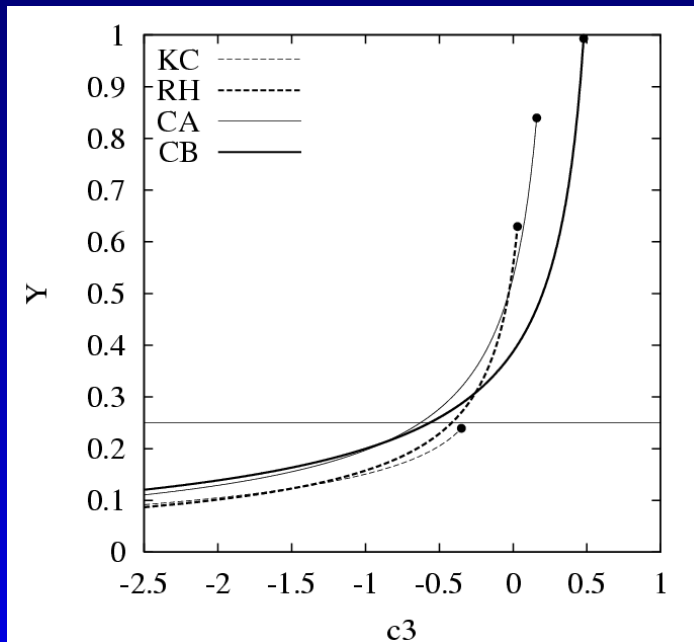
$$k^{n-1} \varepsilon^m (c_{nm1} P + c_{nm3} B - c_{nm2} \varepsilon)$$

This works without correction term only for  $m \geq 0$ .

# Total equilibrium ( $k$ - $\varepsilon$ )

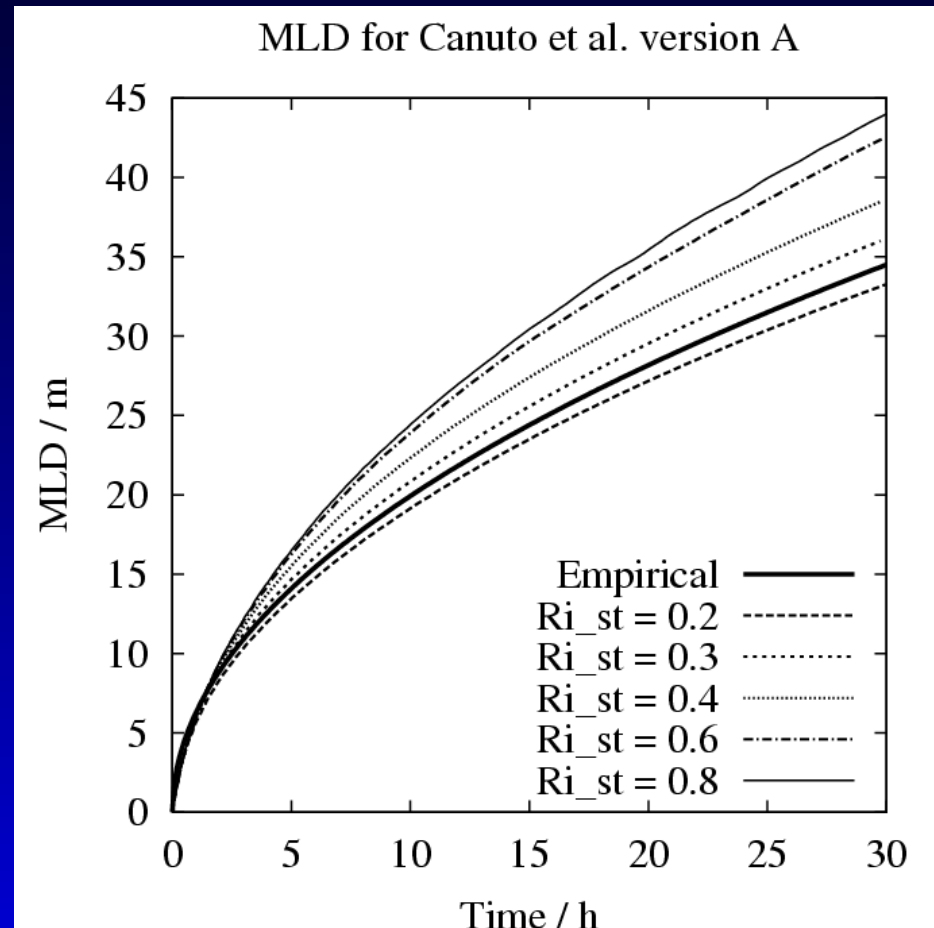
$$\dot{k} = \dot{\varepsilon} \implies R_i = \frac{-\frac{g}{\rho_0} \partial_z \rho}{(\partial_z u)^2 + (\partial_z v)^2} = R_i^{st} = \frac{c_\mu}{c'_\mu} \cdot \frac{c_{2\varepsilon} - c_{1\varepsilon}}{c_{2\varepsilon} - c_{3\varepsilon}}.$$

$R_i^{st} \approx 0.25$ : Steady-state Richardson number.



# Kato-Phillips experiment

## Wind-induced mixed-layer depth (MLD)




Burchard & Bolding [2001]

GOTM (General Ocean Turbulence Model) - Microsoft Internet Explorer

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**Challenge**


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- [The Idea](#)
- [Key features](#)

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# General Ocean Turbulence Model

GOTM is a one-dimensional numerical model developed and supported by a [core team](#) of ocean modellers. GOTM aims at simulating accurately [vertical exchange processes](#) in the marine environment where [mixing](#) is known to play a key role. GOTM is freely available under the [GPL](#) (Gnu Public License).

If you are interested in using GOTM, you can download:

Software: [Fortran source](#)

Examples: [Test cases - Outputs](#)

Documentation: [Summary](#) - [2003 report](#) - [1999 report](#)

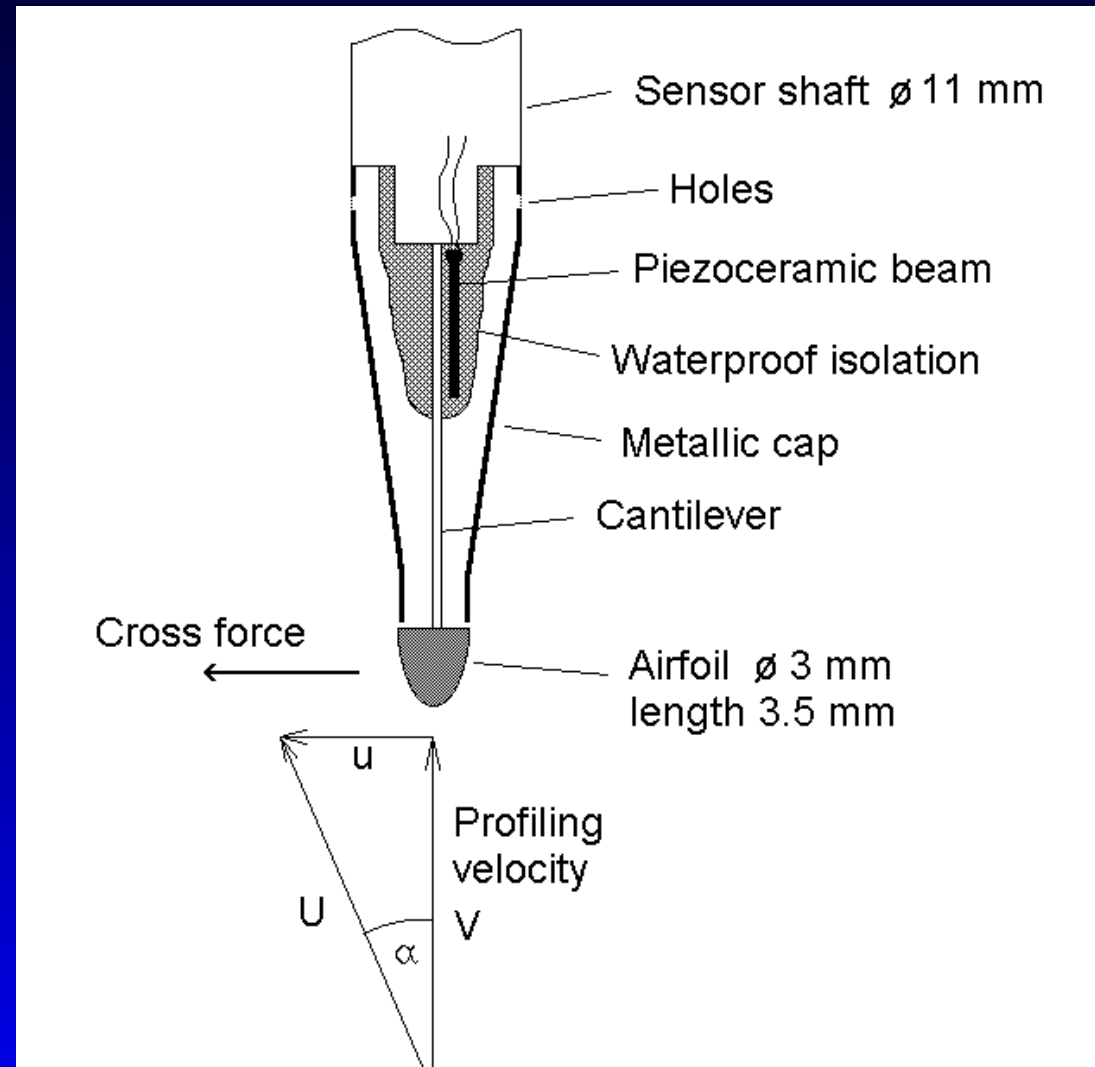
You are warmly invited to join the [GOTM mailing list](#) and send any comments/questions to the [GOTM developers](#) or become a [GOTM contributor](#). The GOTM developers are grateful to their [sponsors](#).

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Last updated: 03/16/2003 09:42:06

# Microstructure observations

Shear probe mounted on free-falling profiler



# Microstructure observations

Definition of dissipation rate:

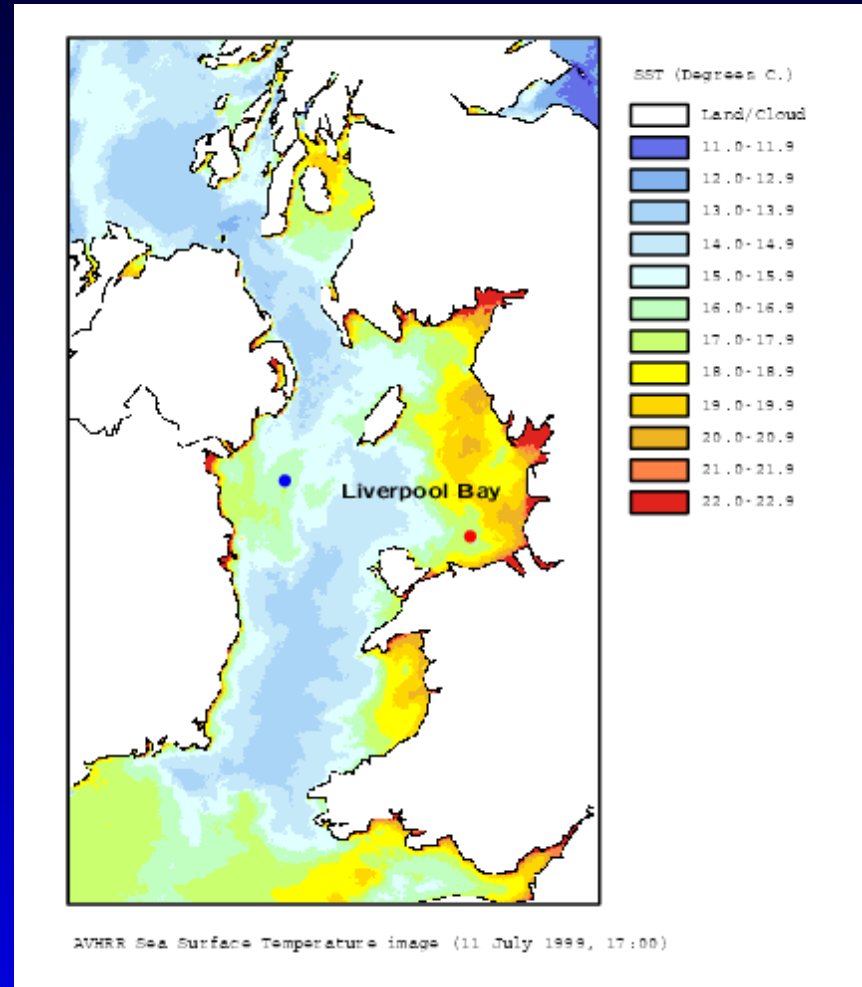
$$\varepsilon = \nu \sum_{i,j=1}^3 \left\langle \left( \frac{\partial \tilde{v}_i}{\partial x_j} \right)^2 \right\rangle$$

Turbulence isotropic at small scales:

$$\varepsilon = 7.5 \nu \left\langle \left( \frac{\partial \tilde{u}}{\partial z} \right)^2 \right\rangle$$

# Liverpool Bay

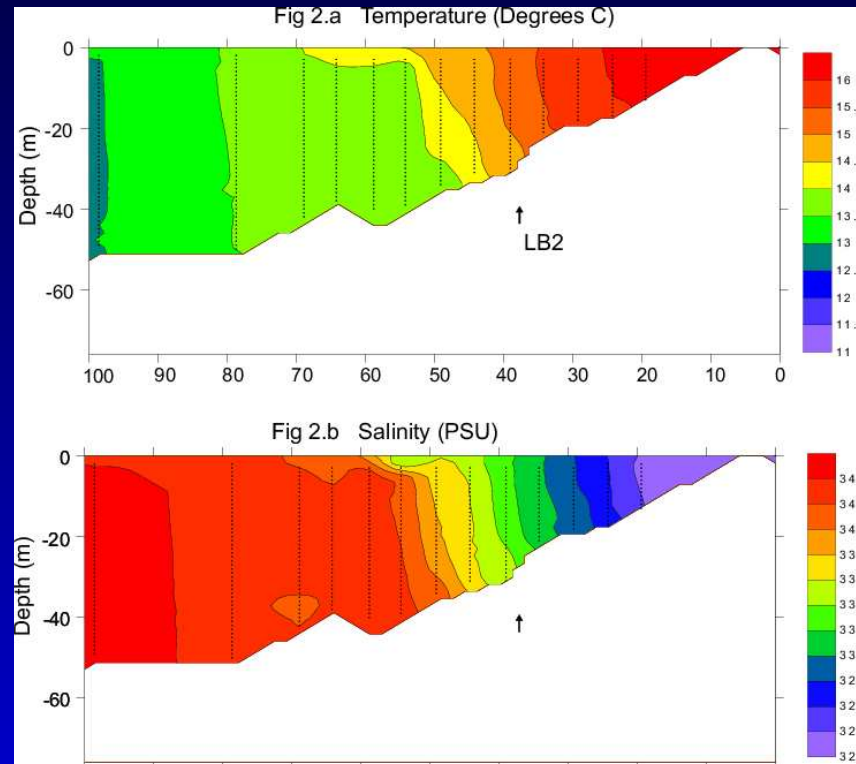
SST from space and location of station (●)



Courtesy to School of Ocean Sciences, UBW, Wales

# Liverpool Bay

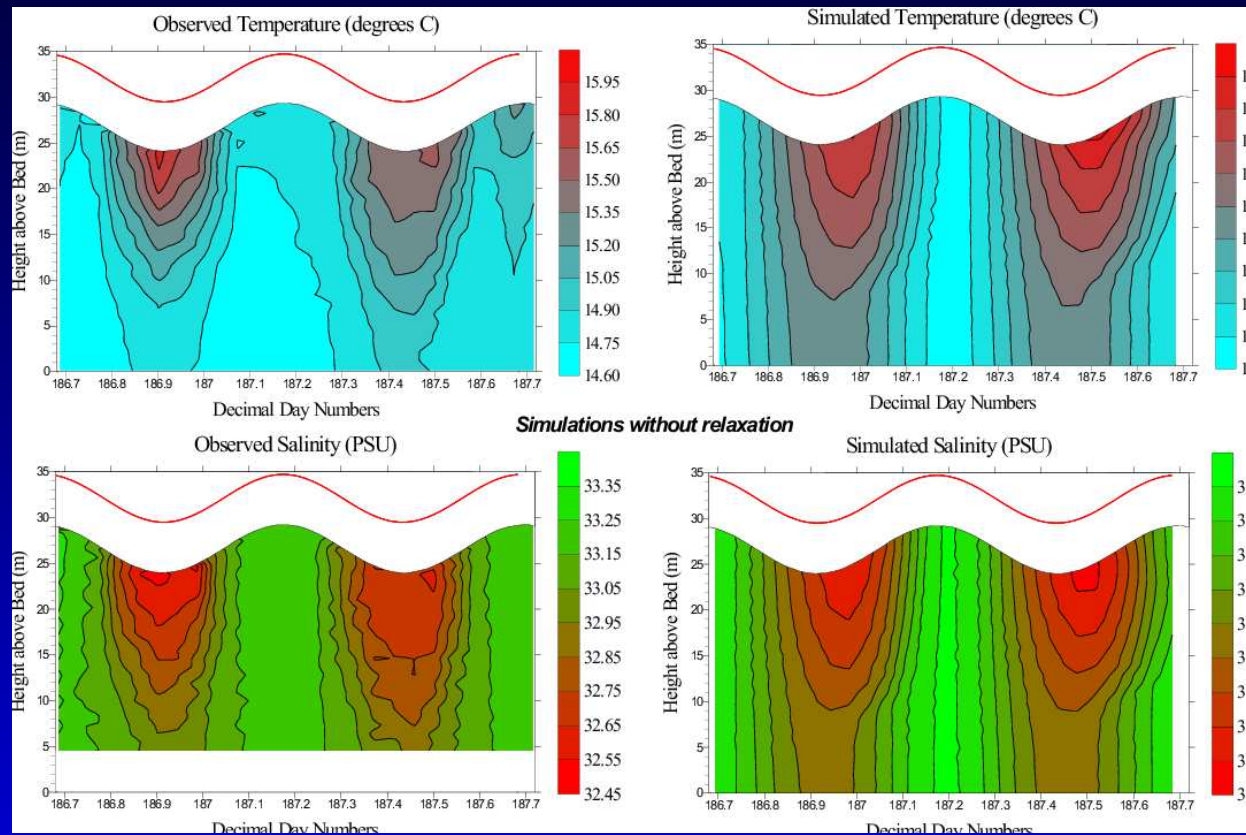
## Section of Temperature and Salinity



Rippeth, Fisher, Simpson [2001]

# Liverpool Bay

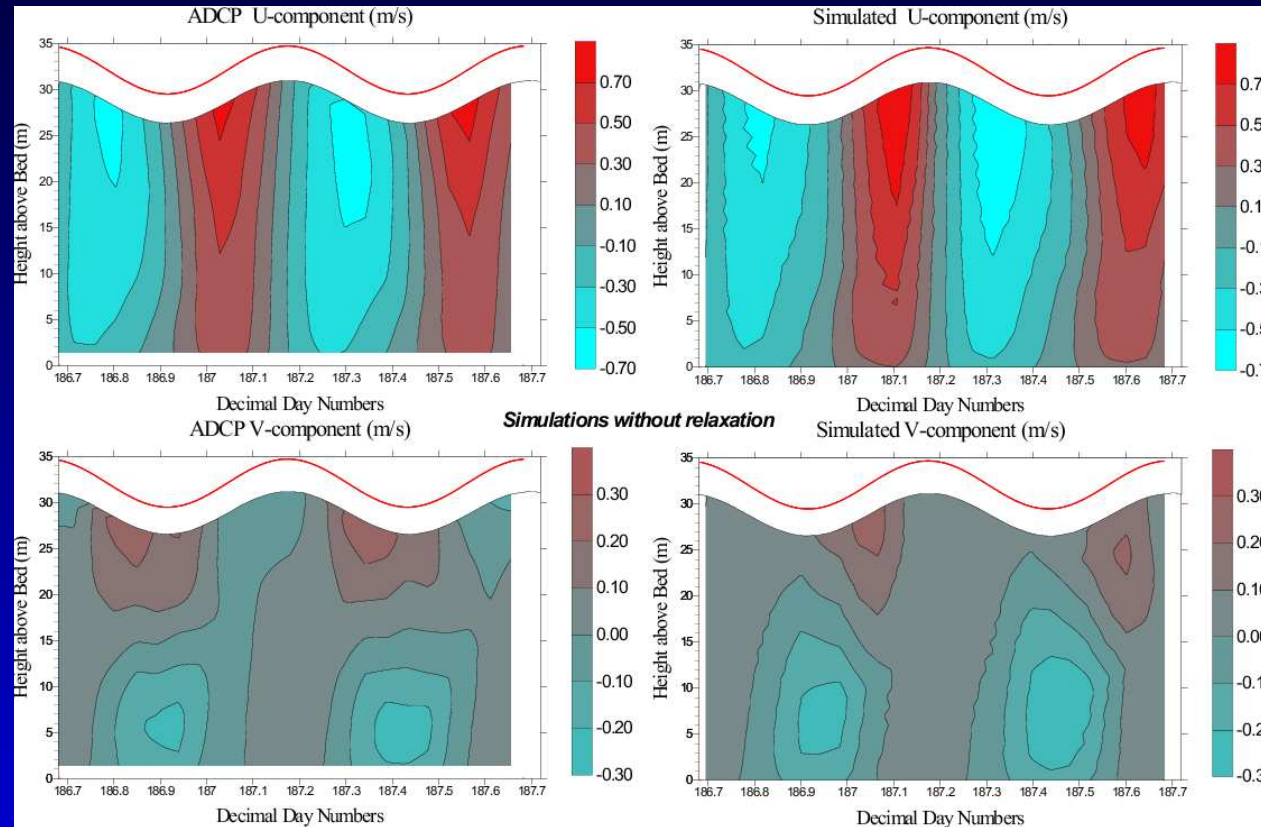
## Observed and simulated temperature and salinity



Simpson, Burchard, Fisher, Rippeth [2002]

# Liverpool Bay

## Observed and simulated current velocity

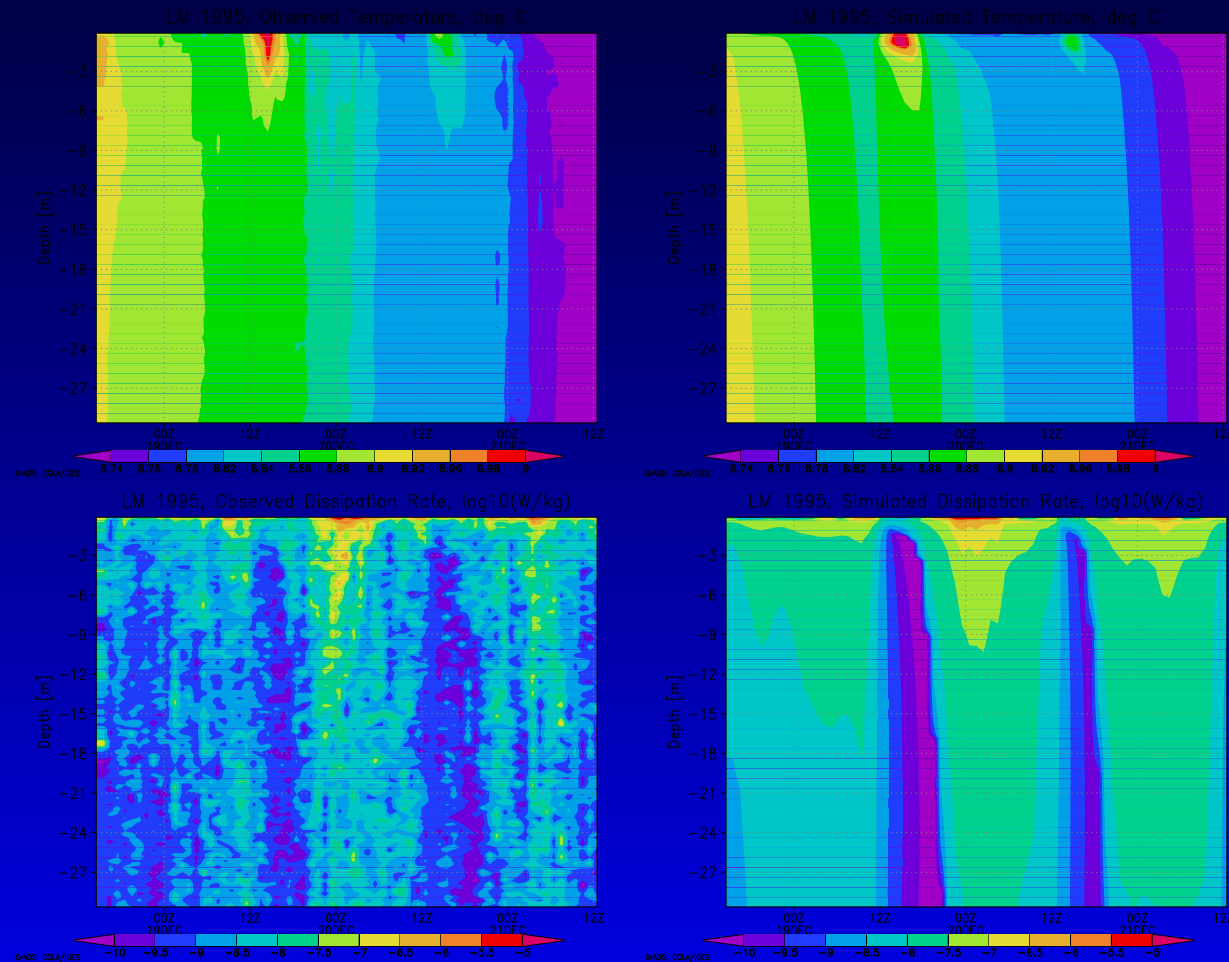


Simpson, Burchard, Fisher, Rippeth [2002]



# Lago Maggiore, Italy

Observations and simulations of  $T$  and  $\varepsilon$  (Stips et al. [2002])

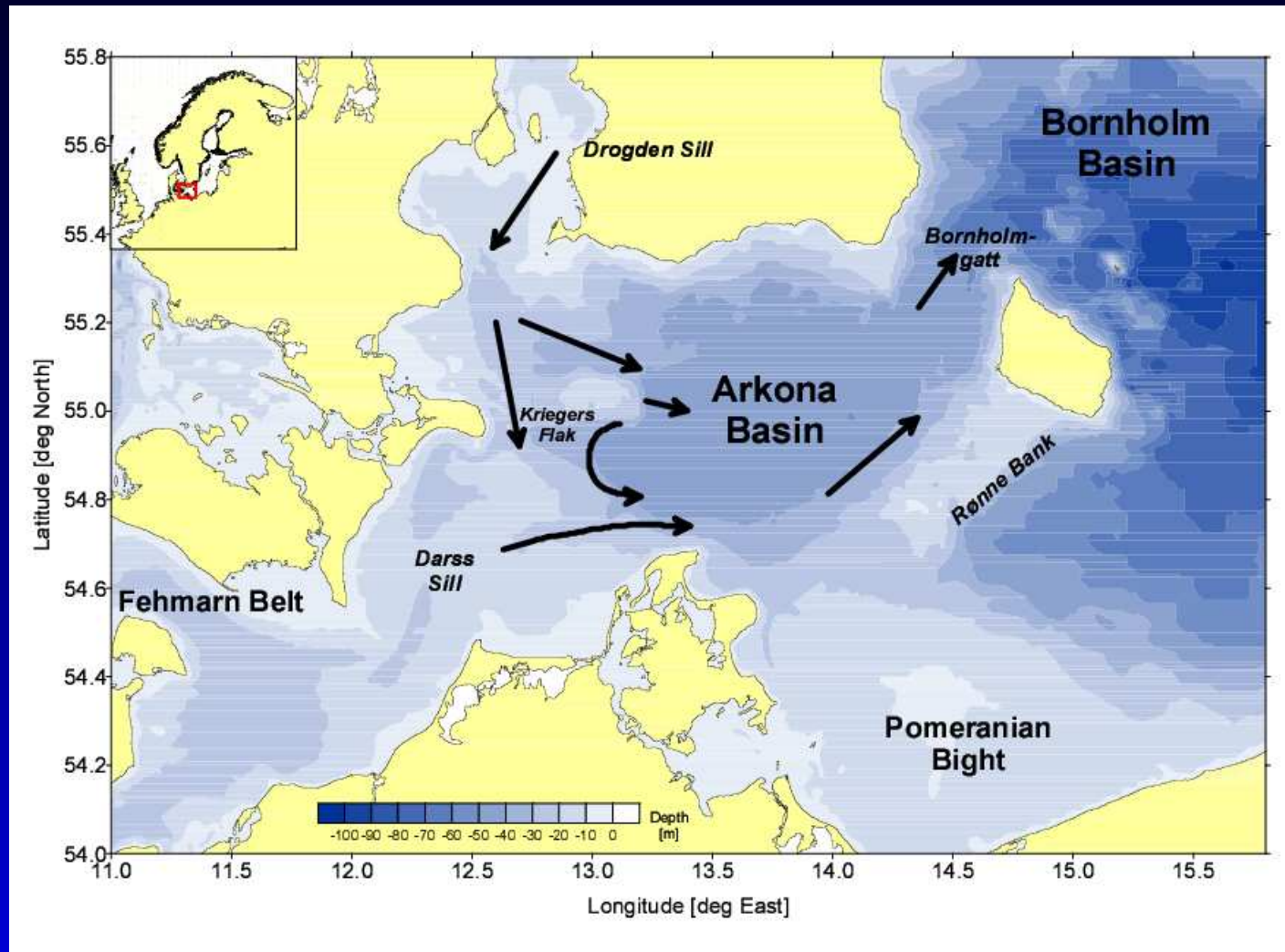




## General Estuarine Transport Model

- Three dimensional, hydrostatic, free surface, baroclinic
- Mode-splitting, Arakawa-C grid
- Horizontal coord.: Cartesian, spherical or orthogonal
- Vertical coord.: Sigma, z-levels or generalised
- Turbulence closures from GOTM (<http://www.gotm.net>)
- Various advection schemes for momentum and tracers
- Stable drying and flooding algorithm
- Fully parallelised (domain decomposition)
- Public Domain (<http://www.bolding-burchard.com/getm>)

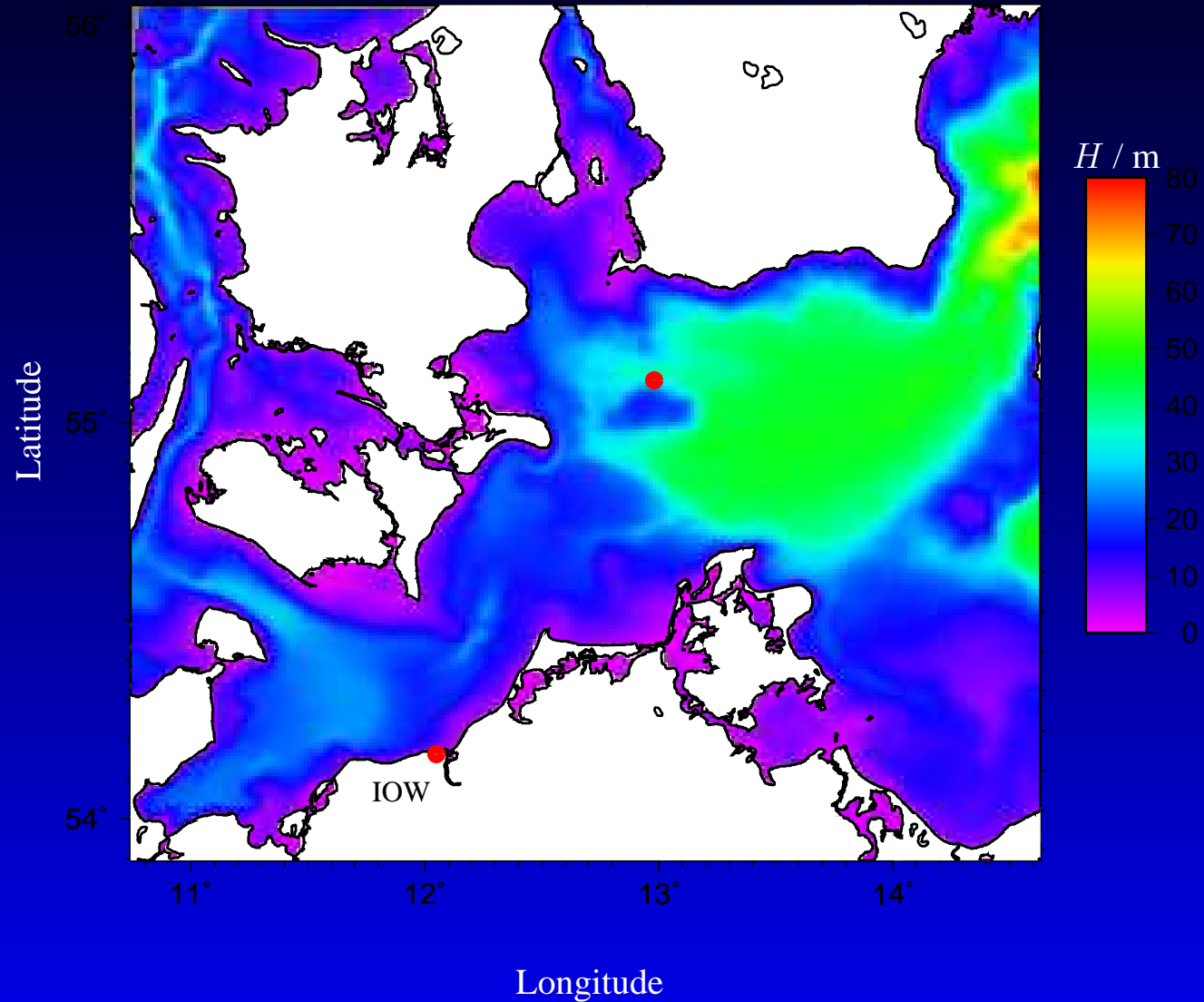
# Arkona Sea



Graphics by Volker Mohrholz, IOW

# Arkona Sea

Model bathymetry

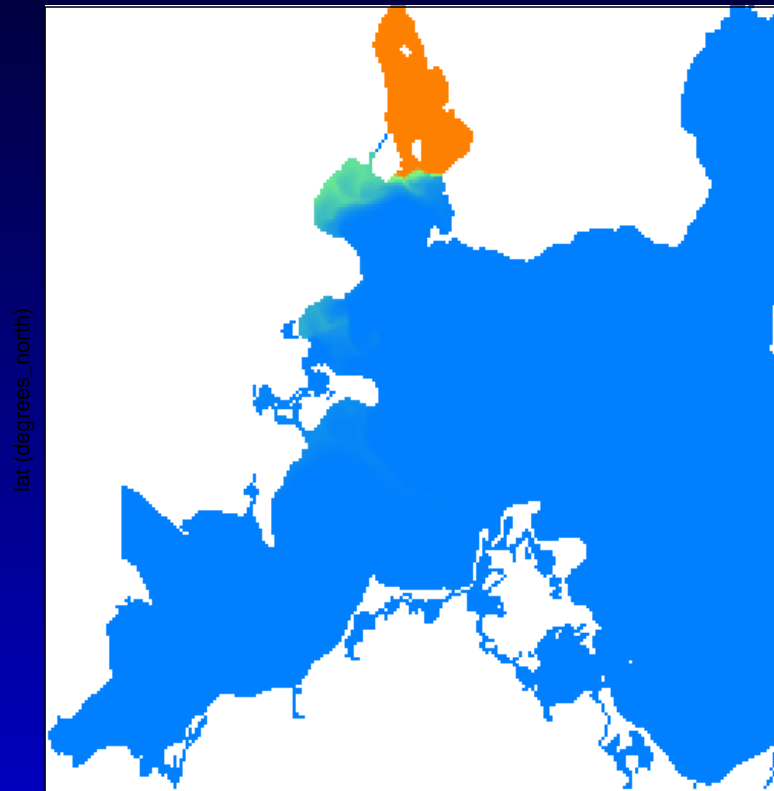


●: QuantAS station

# Arkona Sea

Surface salinity (8-25 psu)

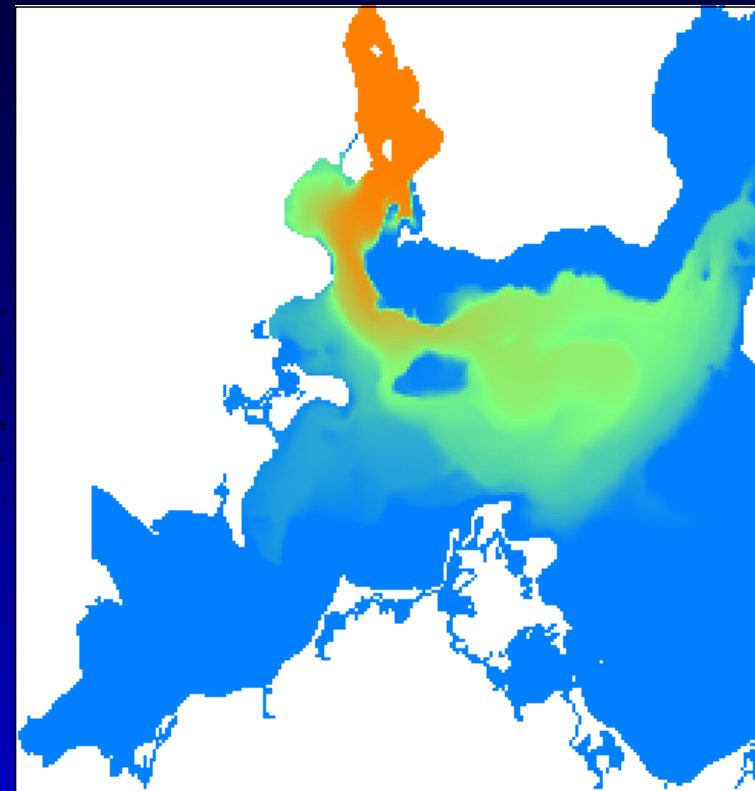
surface salinity (PSU)



lon (degrees\_east)

Bottom salinity (8-25 psu)

bottom salinity (PSU)

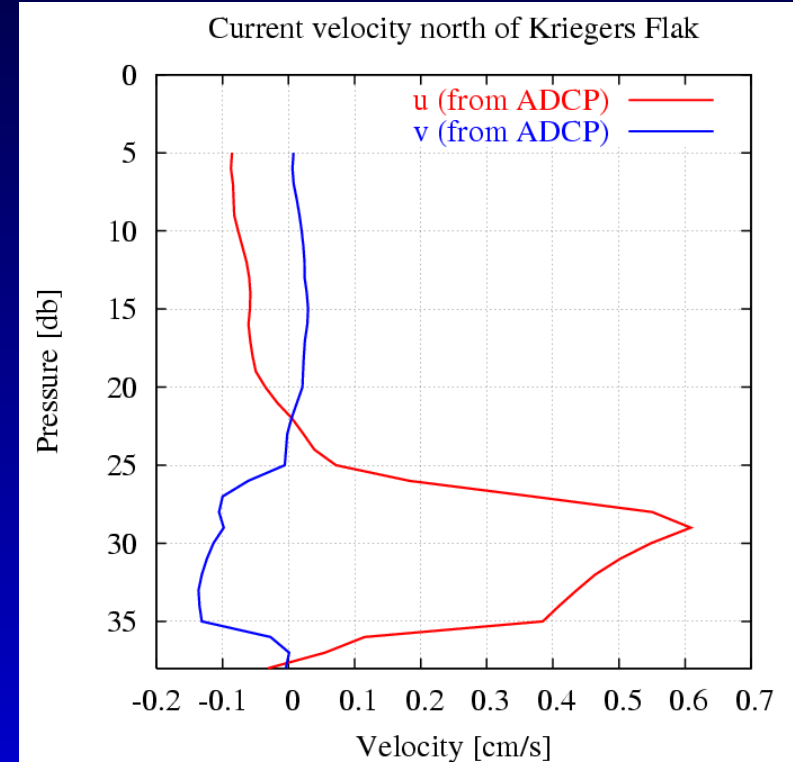
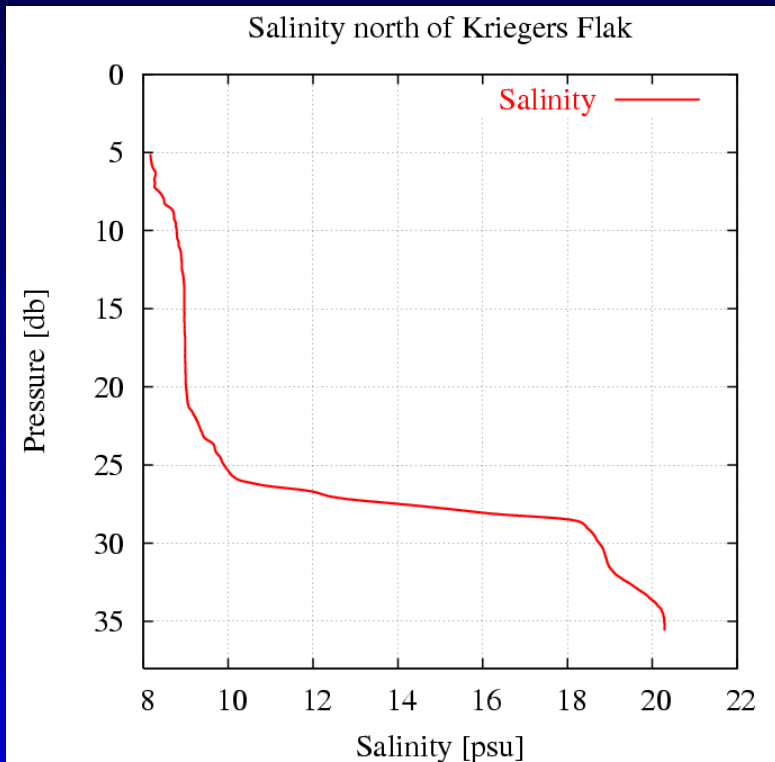


lon (degrees\_east)

Simulation with GETM

# Arkona Sea

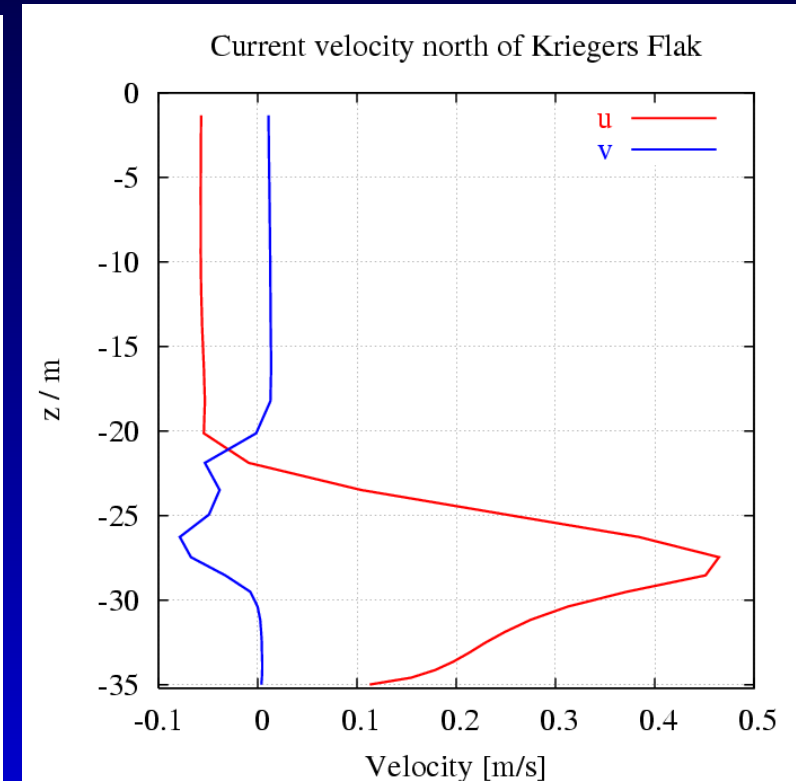
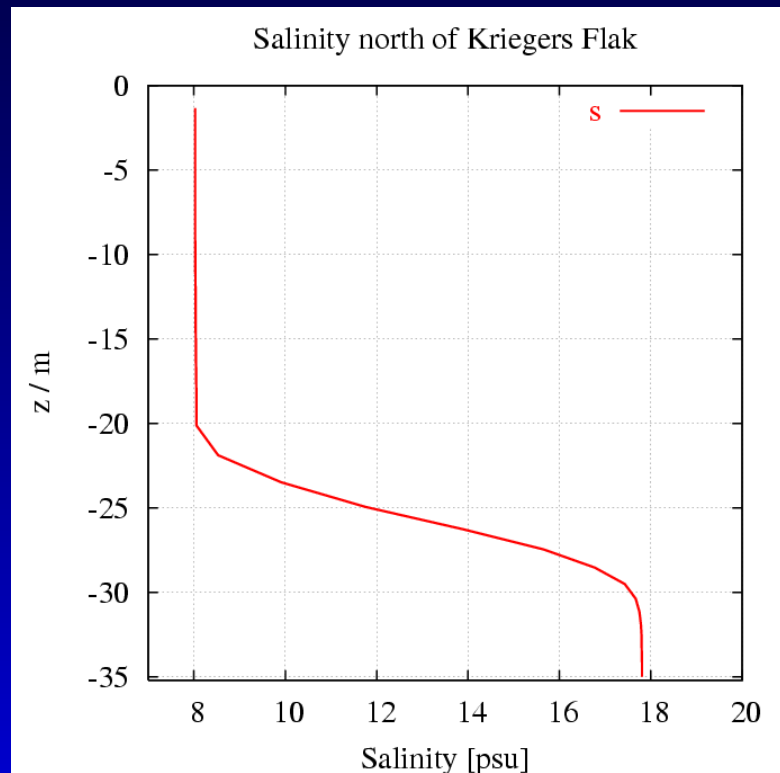
Observations from moored ship (MzB Helmsand)



Data by Jürgen Sellschopp, Volker Fiekas, FWG Kiel

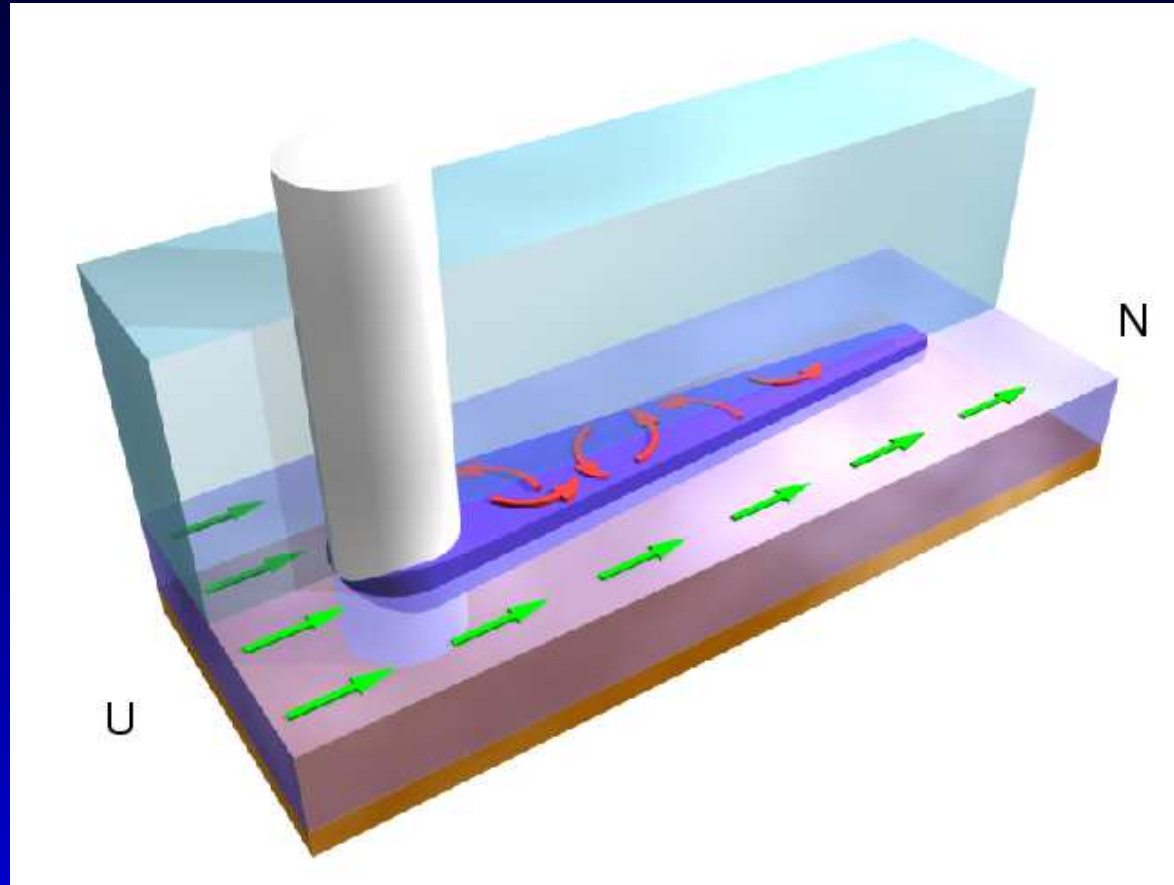
# Arkona Sea

Idealised simulations (with GETM)



# Offshore Constructions

Additional mixing by Offshore Wind Farms ?



Graphics by Jan Donath (IOW)

# Conclusions

Quantitative numerical simulations of buoyancy effects in the coastal zone require models with certain properties such as

- Higher turbulence closures
- Surface and bottom following coordinates
- Positive definite and monotone advection schemes

Advantageous are highly flexible vertical and horizontal coordinates.

# Thanks to ...

- Karsten Bolding (BBH)
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