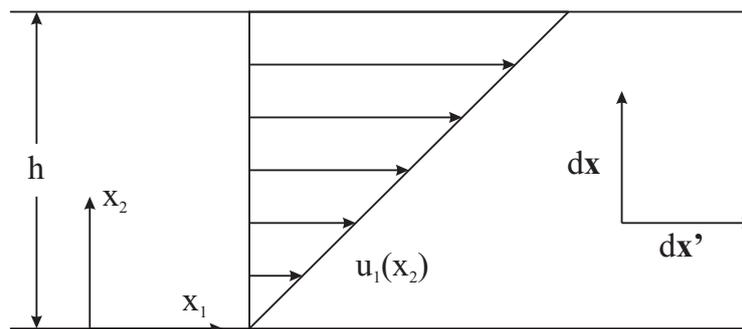


Assignment Nr. 3

due November 22th

Problem 1



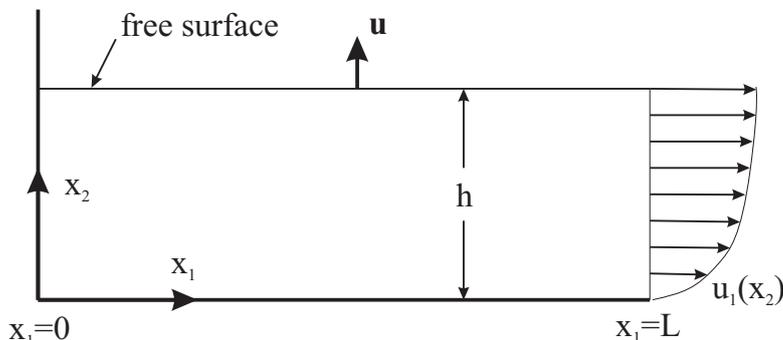
Consider a shear flow between two tangentially moving plates (Couette flow) with velocity given by

$$u_1 = \frac{U}{h}x_2, \quad u_2 = u_3 = 0,$$

where U is the constant velocity difference between the moving plates, and h their constant distance.

- (a) Compute the components of the velocity gradient, $\partial u_i / \partial x_j$, in Cartesian coordinates. Use the result to compute the symmetric and anti-symmetric parts, S_{ij} and W_{ij} , of the velocity gradient. Here and in the following, it is sufficient to write down all expressions in two dimensions (x_1, x_2) only.
- (b) Compute the rate of strain of the two line elements, $d\mathbf{x}$ and $d\mathbf{x}'$, oriented in the x_2 and x_1 directions, respectively.
- (c) Compute the rate at which the angle between the two line elements changes (shear rate).
- (d) Compute the average angular velocity of the two line elements (rotation rate).
- (e) Compute the eigenvalues and eigenvectors of the rate of deformation tensor, S_{ij} . What is the angle between these eigenvectors and the x -axis? (Hint: it is sufficient to consider only the 2 by 2 matrix of the plane problem in the x_1 and x_2 directions. Since S_{ij} is real and symmetric, the two eigenvectors are orthogonal.)
- (f) What is the significance of the two directions given by the two eigenvectors? How do you think two infinitesimal line elements pointing in these directions are deformed?

Problem 2



The figure shows an estuary (like the Elbe river mouth) with idealized geometry. It consists of a channel of length L that is closed by a vertical wall at $x_1 = 0$ and has an open boundary with the ocean at $x_1 = L$. The flat bottom of the estuary is located at $x_2 = 0$ and the free surface at $x_2 = h$. Due to tidal motions, the position of the horizontal free surface, $h(t)$, is a function of time, t . It is assumed to be described by the formula

$$h(t) = h_0 + a \sin \frac{2\pi t}{T} , \quad (1)$$

where h_0 is the mean water level, a the amplitude of the tide, and T the tidal period. Assume that at $x_1 = L$, the profile of the horizontal velocity is given by

$$u_1(x_2) = U(t) \ln \left(\frac{x_2 + z_0}{z_0} \right) , \quad (2)$$

with $U(t)$ defining an unknown function of time. This is a typical profile for a turbulent channel flow, where the so-called “bottom roughness”, z_0 , is assumed to be known.

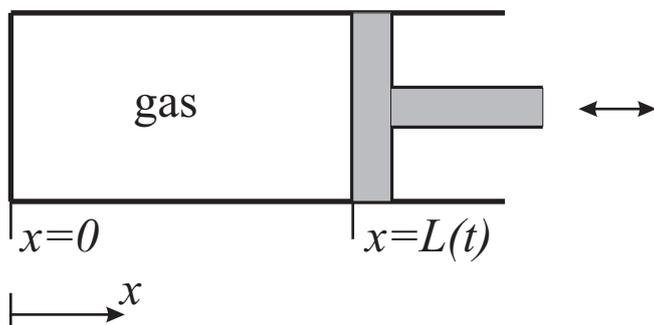
- (a) Show that for homogeneous, constant density, $\rho = \rho_0$, the integral form of the balance of mass can be written as

$$\int_A \mathbf{u} \cdot \mathbf{n} \, dA = 0 , \quad (3)$$

where the surface, A , consists of the bottom, the left closed boundary, the right open boundary, and the free surface.

- (b) Evaluate (3) formally, taking into account all four surfaces.
(c) From the solution of (3), derive an expression for the function $U(t)$ in (2).
(d) Use this result to plot profiles of the velocity $u_1(x_2)$ at $x_1 = L$ for $t = T/4$, $T/2$, $3T/4$, and T , using the following numerical values: $L = 100$ km, $h_0 = 50$ m, $a = 5$ m, $z_0 = 0.01$ m, and $T = 12.42$ h. This corresponds to a typical semi-diurnal tide in some estuaries in the North Sea.

Problem 3



Consider a cylindrical tube with constant cross-sectional area, A , that is filled with a compressible gas. The tube is closed at the left end, $x = 0$, such that the gas can be compressed by a moving piston located at $x = L(t)$. The position of the piston is a function of time, t , and assumed to be given by

$$L(t) = \frac{L_0}{2 - \cos \omega t} , \quad (4)$$

where the constant angular velocity, ω , and the constant reference position, L_0 , are known.

- (a) Assuming that the density ρ only depends on t and x , show that the integral balance of mass for the material volume of gas inside the tube is given by

$$\frac{d}{dt} \int_0^{L(t)} \rho \, dx = 0 \quad . \quad (5)$$

- (b) Show that *one* possible solution of (5) corresponds to

$$\rho = \rho_0(2 - \cos \omega t) , \quad (6)$$

where ρ_0 is an arbitrary, but constant reference density (hint: use Leibniz' integration rule). This solution is valid only if the speed of the piston, \dot{L} , is small compared to the speed of sound. In this case, no sound waves are generated by the piston, and ρ can be assumed to be homogeneous.

- (c) Show that for one-dimensional problems, like the one at hand, the general form of the local balance of mass adopts the simple form

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0 \quad . \quad (7)$$

- (d) Insert (6) into (7) to obtain an expression for the divergence of the velocity, which is $\partial u / \partial x$ in one-dimensional flows. Integrate the expression for $\partial u / \partial x$ to obtain the spatial distribution of the velocity, $u(x, t)$, inside the tube. Note that at the closed end $u(0, t) = 0$.

- (e) Plot L , ρ , and the divergence of the velocity, $\partial u / \partial x$, for $0 \leq t \leq 2\pi$ for $L_0 = \rho_0 = 1$, and $\omega = 2$. Mark periods of positive divergence and periods of decreasing density. Do these periods coincide? Should they?